



# BOWLING GREEN VERTICAL CONTROL NETWORK (BGVCN)

THE CITY OF BOWLING GREEN

June 2009

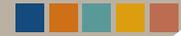


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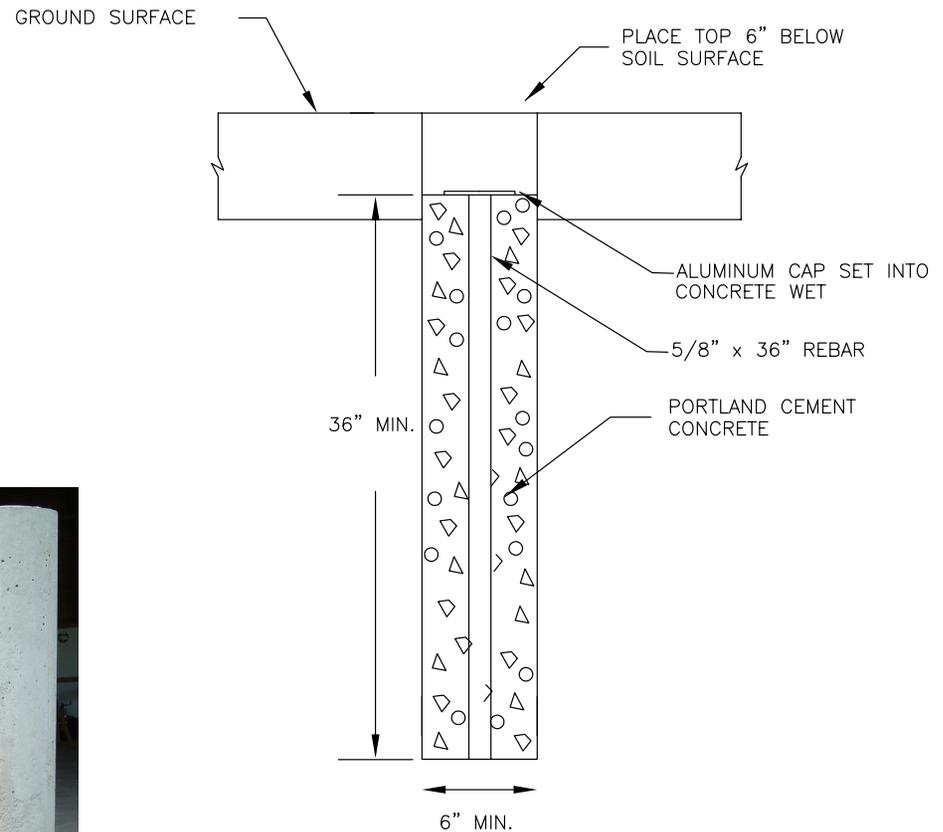
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# INTRODUCTION



This report by **Poggemeyer Design Group** (PDG) is to summarize professional surveying services prepared for The City of Bowling Green for the Bowling Green Vertical Control Network (BGVCN). PDG has completed all of the fieldwork and calculations required to report elevations on fifteen (15) concrete monuments surrounding Bowling Green, Ohio.

The BGVCN meets the National Geodetic Survey's current Elevation Accuracy Standards for a Second Order-Class II Vertical Control Network. This Vertical Control Network consists of fifteen (15) existing monuments, previously constructed by BG or others, and four (5) existing First Order-Class II monuments, previously maintained by National Geodetic Survey (NGS). There is no anticipation to "Blue Book" any of the fifteen BGVCN monuments to the NGS database. This report will briefly outline the technical approach and calculations performed on this project.



VERTICAL MONUMENT DETAIL	
CITY OF BOWLING GREEN PUBLIC WORKS DEPARTMENT ENGINEERING DIVISION	STD DWG
	SH 1 OF 1
	REV 10/2008



## Personnel

- Dana A. Parsell, P.S. – Project Manager
- Michael A. Horn, P.S.
- John C. Bair
- Jordan M. Atherine
- Kevin H. Mielnik

## Equipment

- Trimble DiNi Digital Level (0.3mm per km)
  - Part No: 7 8030 017
  - Manufactured: 2009
  - Serial No. 708274
- Two (2) Staffs – Trimble Invar Rod LD 13 with bipods
  - Each staff is a three (3) meter, code-graduated rod.
- Two (2) Footplates with steel punch
  - Footplates used for turning points at each station.
- One (1) Trimble 5800 dual-frequency GPS receiver with Trimble TSC2 data collector.
  - Motorola i580 cellular phone to connect to Ohio Department of Transportation (ODOT) Virtual Reference System.
  - GPS receiver used for reconnaissance, recovery, and review of existing monumentation.

## Level Loop Routes

PDG planned, coordinated, and performed three (3) level loops routes. This route was pre-approved by National

Geodetic Survey prior to performing any fieldwork for this project.

### Route No. 1

Lineal Distance 51,204 feet +/-

Closure 0.041 feet

### Route No. 2

Lineal Distance 80,006 feet +/-

Closure 0.054 feet

### Route No. 3

Lineal Distance 51,081 feet +/-

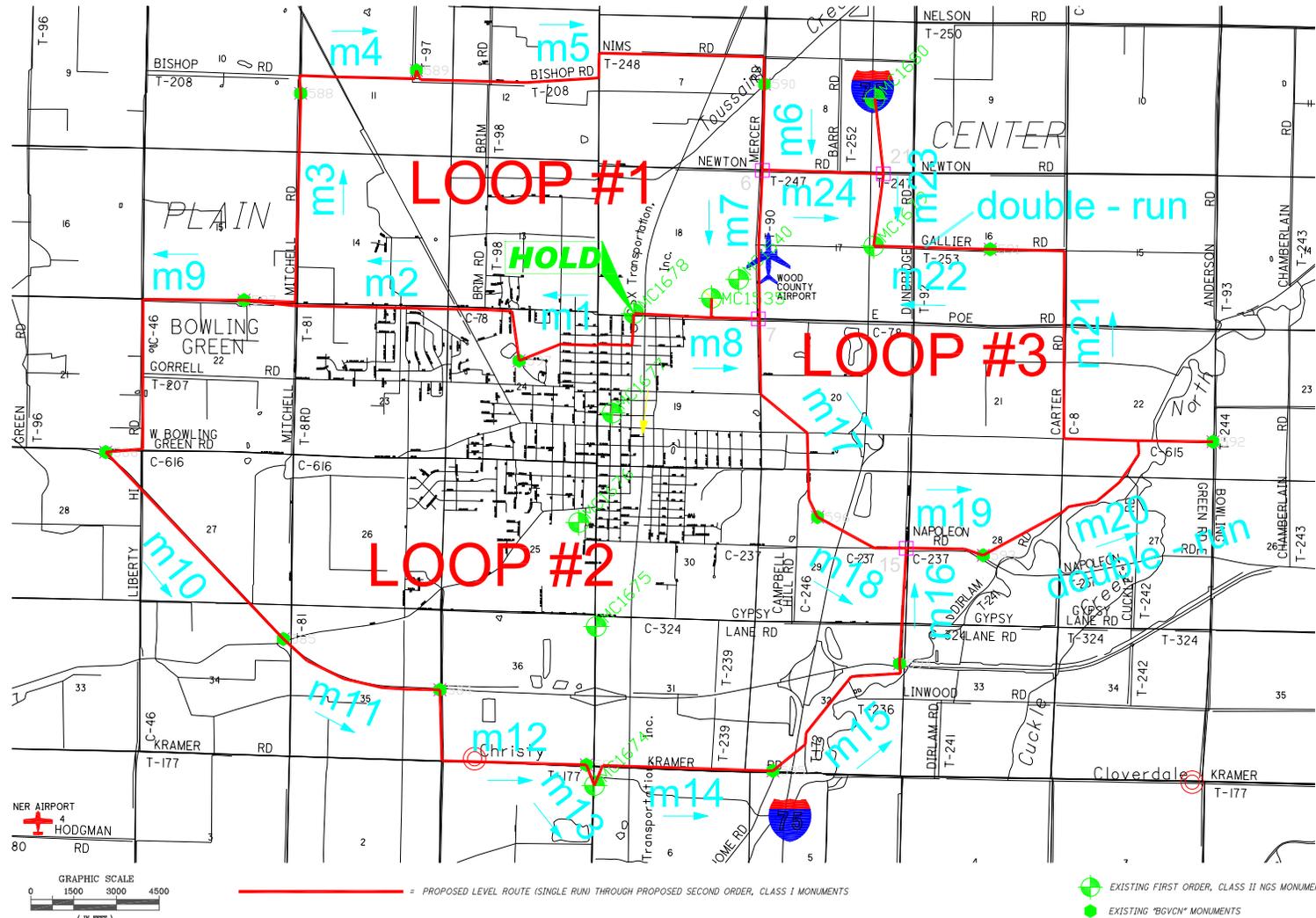
Closure 0.057 feet\*

\* Note: Part of this route was double-run to check existing measurements, verify measurement ties to existing vertical control, and minimize errors in the overall adjustment.

# CALCULATIONS



PDG compiled the survey data and performed a Least Squares Adjustment (LSA) of the survey information.



**A Priori Data:** As directed by The City of Bowling Green, all survey data is to be referenced to the following existing NGS monument: (See NGS Data Sheet attached)

**PID**  
MC1678

**DESIGNATION**  
C351

**NAVD 88**  
675.00'

**MONUMENT**  
Stainless Steel Rod  
in Sleeve



# CALCULATIONS



## Variance / Covariance Matrix and Weight Matrix

We need to assign residual ( $\Phi$ ) and variance ( $\Phi^2$ ) values for the precisions of each measurement. Please note, PDG has conservatively estimated the precisions of each measurement for the purpose of providing weight in this adjustment. For this project, we have used the following values:

- m1 thru m20 .....residual ( $\Phi$ ) = 0.05'                      variance ( $\Phi^2$ ) = 0.0025'
- m21 .....residual ( $\Phi$ ) = 0.20'                                variance ( $\Phi^2$ ) = 0.04'
- m22 thru m24 .....residual ( $\Phi$ ) = 0.05'                      variance ( $\Phi^2$ ) = 0.0025'
- m25 and m26 .....residual ( $\Phi$ ) = 0.005'                      variance ( $\Phi^2$ ) = 0.000025'

V = Variance / Covariance matrix

Cov. :=

	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	
0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
1	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.04	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5·10 <sup>-3</sup>	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5·10 <sup>-5</sup>	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.5·10 <sup>-5</sup>

# CALCULATIONS



## Variance / Covariance Matrix and Weight Matrix

$V^{-1}$ = Weight matrix

$Cov^{-1}$

	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	
0	400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1	0	400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	0	0	400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	400	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	400	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	400	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	400	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	400	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	400	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	400	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	400	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	400	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	25	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	400	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	400	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	400	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	$4 \cdot 10^4$
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

# CALCULATIONS



## Normal Equations

$$(B^T * V^{-1} * B) * X = B^T * V^{-1} * M$$

## Solving for X:

$$X = (B^T * V^{-1} * B)^{-1} * (B^T * V^{-1} * M)$$

$B^T =$

	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25
0	1	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1	0	1	-1	0	0	0	0	0	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	0	0	1	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	1	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	1	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	1	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-1	0	0
6	0	0	0	0	0	0	1	1	0	0	0	0	0	0	0	0	-1	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	1	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	1	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	1	-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	1	-1	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	1	-1	0	0	0	0	0	0	0	0	0	0	0	1
12	0	0	0	0	0	0	0	0	0	0	0	0	0	1	-1	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	-1	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	-1	-1	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	-1	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	-1	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	-1	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	0	1	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-1	1	0	0

$B^T$

# CALCULATIONS



## Normal Equations

M = M measured

m1	=	X1-HA	=	678.022'
m2	=	X2-X1	=	-3.202'
m3	=	X3-X2	=	-1.780'
m4	=	X4-X3	=	0.384'
m5	=	X5-X4	=	-3.138'
m6	=	X6-X5	=	1.693'
m7	=	X7-X6	=	3.193'
m8	=	X7-HA	=	675.131'
m9	=	X8-X2	=	0.158'
m10	=	X9-X8	=	14.355'
m11	=	X10-X9	=	-3.561'
m12	=	X11-X10	=	-2.399'
m13	=	X12-X11	=	-1.464'
m14	=	X13-X12	=	-5.126'
m15	=	X14-X13	=	-7.301'
m16	=	X15-X14	=	4.451'
m17	=	X16-X7	=	-1.255'
m18	=	X15-X16	=	0.003'
m19	=	X17-X15	=	-4.139'
m20	=	X18-X17	=	-2.5385'
m21	=	X19-X18	=	1.500'
m22	=	X20-X19	=	0.140'
m23	=	X20-X21	=	1.272'
m24	=	X21-X6	=	-4.473'
m25	=	X20-HA	=	668.74'
m26	=	X12-HA	=	681.87'

Solving for X:

$$X = (B^T * V^{-1} * B)^{-1} * (B^T * V^{-1} * M)$$

$$x := [(B^T) \cdot Cov \cdot B]^{-1} \cdot (B^T \cdot Cov \cdot meas)$$

	0					
0	678.014	X1	=	678.014'	=	Point #597
1	674.805	X2	=	674.805'	=	Point #587
2	673.024	X3	=	673.024'	=	Point #588
3	673.407	X4	=	673.407'	=	Point #589
4	670.268	X5	=	670.268'	=	Point #590
5	671.96	X6	=	671.960'	=	Point TP6
6	675.138	X7	=	675.138'	=	Point TP3
7	674.956	X8	=	674.956'	=	Point #586
8	689.305	X9	=	689.305'	=	Point #585
9	685.737	X10	=	685.737'	=	Point #584
10	683.332	X11	=	683.332'	=	Point #583
11	681.861	X12	=	681.861'	=	Point #MC
12	676.729	X13	=	676.729'	=	Point #595
13	669.421	X14	=	669.421'	=	Point #594
14	673.866	X15	=	673.866'	=	Point TP4
15	673.876	X16	=	673.876'	=	Point #596
16	669.713	X17	=	669.713'	=	Point #593
17	667.16	X18	=	667.160'	=	Point #592
18	668.659	X19	=	668.659'	=	Point #591
19	668.786	X20	=	668.786'	=	Point #MC
20	667.5	X21	=	667.500'	=	Point TP2

# CALCULATIONS



## Normal Equations

B * x	=	Mc corrected	Mc corrected	-	M measured	=	Δ adjustment
Mc1	=	678.013'	678.013'	-	678.022'	=	-0.008561'
Mc2	=	-3.211'	-3.211'	-	-3.202'	=	-0.008561'
Mc3	=	-1.784'	-1.784'	-	-1.780'	=	-0.004195'
Mc4	=	0.380'	0.380'	-	0.384'	=	-0.004195'
Mc5	=	-3.142'	-3.142'	-	-3.138'	=	-0.004195'
Mc6	=	1.689'	1.689'	-	1.693'	=	-0.004195'
Mc7	=	3.191'	3.191'	-	3.193'	=	-0.002238'
Mc8	=	675.136'	675.136'	-	675.131'	=	0.004861'
Mc9	=	0.154'	0.154'	-	0.158'	=	-0.004367'
Mc10	=	14.351'	14.351'	-	14.355'	=	-0.004367'
Mc11	=	-3.565'	-3.565'	-	-3.561'	=	-0.004367'
Mc12	=	-2.403'	-2.403'	-	2.399'	=	-0.004367'
Mc13	=	-1.468'	-1.468'	-	-1.464'	=	-0.004367'
Mc14	=	-5.130'	-5.130'	-	-5.126'	=	-0.003646'
Mc15	=	7.305'	7.305'	-	-7.301'	=	-0.003646'
Mc16	=	4.447'	4.447'	-	4.451'	=	-0.003646'
Mc17	=	-1.252'	-1.252'	-	-1.255'	=	0.002623'
Mc18	=	0.004'	0.004'	-	0.003'	=	-0.002623'
Mc19	=	-4.140'	-4.140'	-	-4.139'	=	-0.001023'
Mc20	=	-2.540'	-2.540'	-	-2.5385'	=	-0.001023'
Mc21	=	1.398'	1.398'	-	1.500'	=	0.102000'
Mc22	=	0.139'	0.139'	-	0.140'	=	-0.001023'
Mc23	=	1.270'	1.270'	-	1.272'	=	-0.001956'
Mc24	=	-4.475'	-4.475'	-	-4.473'	=	-0.001956'
Mc25	=	668.740'	668.740'	-	668.740'	=	0.000186'
Mc26	=	681.870'	681.870'	-	681.870'	=	0.000045'

# SUMMARY



PDG has completed the Bowling Green Vertical Control Network and reports the following measured data:

POINT	NORTHING	EASTING	LATITUDE	LONGITUDE	DESCRIPTION	ELEVATION
583	612536.466	1652374.869	41°20'32.01937"N	83°39'04.70574"W	KRAMER & US 25	683.332'
584	615168.363	1647234.98	41°20'57.34381"N	83°40'12.54449"W	RT 6 AND RUDOLPH	685.737'
585	616950.271	1641741.745	41°21'14.21263"N	83°41'24.87846"W	RT 6 AND SAND RIDGE	689.305'
586	623498.131	1635511.004	41°22'18.04939"N	83°42'47.76199"W	RT 6 AND BG ROAD	674.956'
587	628825.422	1640362.947	41°23'11.33839"N	83°41'45.09040"W	POE ROAD	674.805'
588	636073.041	1642352.189	41°24'23.20428"N	83°41'20.29320"W	MITCHELL ROAD	673.024'
589	636877.531	1646411.42	41°24'31.69492"N	83°40'27.17320"W	HULL PRAIRIE	673.407'
590	636399.449	1658620.925	41°24'28.56526"N	83°37'46.88130"W	MERCER ROAD/TOUSSAINT	670.268'
591	630607.469	1666547.341	41°23'32.34853"N	83°36'01.91435"W	GALLIER	668.659'
592	623861.225	1674361.516	41°22'26.66439"N	83°34'18.31560"W	BG ROAD & HOUSEKEEPER	667.160'
593	619881.104	1666302.802	41°21'46.35328"N	83°36'03.34599"W	NAPOLEON	669.713'
594	616084.192	1663362.007	41°21'08.47527"N	83°36'41.27311"W	RT 6 AND DUNBRIDGE	669.421'
595	612323.685	1658918.561	41°20'30.76190"N	83°37'38.89163"W	KRAMER & COUNTY HOME	676.729'
596	621219.086	1660486.709	41°21'58.83878"N	83°37'19.83606"W	CARTER PARK	673.876'
597	626701.595	1650019.34	41°22'51.64637"N	83°39'38.05409"W	CITY PARK	678.014'
MC1535	628889.785	1656760.908	41°23'14.14005"N	83°38'10.00402"W	NGS MONUMENT	671.358'
MC1674	611856.349	1652697.962	41°20'25.34266"N	83°39'00.35291"W	NGS MONUMENT	681.861'
MC1678	628356.074	1654038.595	41°23'08.51574"N	83°38'45.62186"W	NGS MONUMENT (HELD)	675.000'
MC1679	630720.225	1662453.226	41°23'32.94857"N	83°36'55.64204"W	NGS MONUMENT	668.786'
MC1680	635875.57	1662588.183	41°24'23.89439"N	83°36'54.73643"W	NGS MONUMENT	667.288'

Coordinate System  
United States State  
Plane 1983  
(ground coordinates)

Zone  
Ohio North (Zone 3401)

Datum Transformation  
NAD 83

Ground Scale factor  
1.0000749645

# APPENDIX 1: DATA SHEETS



# APPENDIX 2: RAW DATA

